

Public reporting burden for this collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing burden, to Washington Headquarters Services, Directorate for Information Operations and Reports, 1215 Jefferson Davis Highway, Suite 1204, Arlington, VA 22202-4302, and to the Office of Management and Budget, Paperwork Reduction Project (0704-0188), Washington, DC 20503.

1. AGENCY USE ONLY (Leave Blank)		2. REPORT DATE 6 September 1996	3. REPORT TYPE AND DATES COVERED Final Technical Report
4. TITLE AND SUBTITLE  Surface Modification of Structural Ceramics By Ion Implantation Annealing: $Al_2O_3$ and $Si_3N_4$		5. FUNDING NUMBERS  Award No. F49620-95-1-0171	
6. AUTHOR(S)  Alan J. Ardell		7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES)  Department of Materials Science and Engineering University of California, Los Angeles 6532 Boelter Hall Los Angeles, CA 90095-1595	
8. SPONSORING/MONITORING AGENCY NAME(S) AND ADDRESS(ES)  Dr. Alexander Pechenik AFOSR/NA 110 Duncan Avenue, Suite B-115 Bolling Air Force Base Washington, D.C. 20332-0001		9. SPONSORING/MONITORING AGENCY REPORT NUMBER  NA F49620- 95-1-0171	
11. SUPPLEMENTARY NOTES			
12a. DISTRIBUTION/AVAILABILITY STATEMENT  Approved for public release, distribution unlimited		12b. DISTRIBUTION CODE  19961016 081	
13. ABSTRACT (Maximum 200 words)  The near-surface regions of polycrystalline $Si_3N_4$ were modified by ion implantation and post-implantation annealing. Metallographically polished bars and disks 3 mm in diameter and ranging in thickness from 250 to 500 $\mu m$ were implanted of co-implanted with $Al^+$ , $B^+$ and $N^+$ to fluences up to $2 \times 10^{16}$ ions/cm <sup>2</sup> , using implantation energies up to 300 keV. Some of the implanted material was post-implantation annealed at temperatures in the neighborhood of 1100 °C. The indentation fracture toughness was found to increase by more than 15 % for certain combinations of fluence, implantation species and post-implantation annealing temperature.			
DTIC QUALITY INSPECTED 4			
14. SUBJECT TERMS  Ion Implantation, Fracture toughness, silicon nitride, Surface modification		15. NUMBER OF PAGES 6	
16. PRICE CODE			
17. SECURITY CLASSIFICATION OF REPORT unclassified	18. SECURITY CLASSIFICATION OF THIS PAGE unclassified	19. SECURITY CLASSIFICATION OF ABSTRACT unclassified	20. LIMITATION OF ABSTRACT

Surface Modification of Structural Ceramics by Ion Implantation and Post-Implantation Annealing:  $\text{Al}_2\text{O}_3$  and  $\text{Si}_3\text{N}_4$

Final Report

Ion implantation experiments were performed on  $\text{Si}_3\text{N}_4$  produced by Cercon Inc., Vista, CA, for the purpose of improving its fracture toughness. The material contained 6 wt. %  $\text{Y}_2\text{O}_3$  and 3 wt. %  $\text{Al}_2\text{O}_3$  as sintering aids, and was HIPped. Pieces measuring  $3 \times 5 \times 5$  mm were cut from the bars provided and metallographically polished in preparation for the first ion implantations. In these experiments specimens of  $\text{Si}_3\text{N}_4$  were implanted individually with  $\text{B}^+$  and  $\text{Al}^+$  or co-implanted with  $\text{B}^+ + \text{N}^+$  and  $\text{Al}^+ + \text{N}^+$ . These choices were dictated primarily by the fact that B and Al are strong nitride formers. The ion implantations were performed at the Hughes Malibu Research Laboratories, using an implanter under the supervision of Dr. R. G. Wilson. The implantation conditions used are summarized in Table 1. The doses were small, but were conveniently attained within a few hours of implantation using the ion beam fluxes available. Post-implantation annealing was done for 24 h at 1000, 1100 and 1200 °C in a  $\text{N}_2$  atmosphere, the purpose of which was to limit the extent of oxidation rather than nitriding the implanted specimens.

The apparent fracture toughness,  $K_c$ , was measured using the indentation-toughness method [1]. This method predicts that  $K_c$  is determined by the equation

$$K_c = \frac{\chi P}{c^{3/2}}, \quad (1)$$

where  $2c$  is the length of the radial/median cracks that originate at the corners of the indentation under load  $P$ . The constant  $\chi$  is obtained from the equation

$$\chi = \delta \left( \frac{E}{H} \right)^{1/2}, \quad (2)$$

where  $E$  is Young's modulus,  $H$  is the Vickers hardness and  $\delta$  is another constant obtained from the equation [2]

$$\delta = \frac{\psi}{24(1-2v)(\sqrt{2}\pi \tan \phi)^{2/3}}, \quad (3)$$

where  $v$  is Poisson's ratio (0.27 for  $\text{Si}_3\text{N}_4$ ),  $2\phi$  is the apex angle of the Vickers indenter and  $\psi$  is another constant determined from the geometry of the crack. When the specimen is large compared to  $c$ ,  $\psi$  takes on the value 1.2 [3-5], which we have used throughout.

Measurements were initially made using an indentation load of 3.5 kg, but at this value of  $P$  the indentation cracks that formed in the annealed specimens were difficult to observe, partly due to limited oxidation of the surface, hence subsequent specimens were indented using  $P = 7.35$  kg (34.3 N). Within the limits of experimental error there were no significant variations of hardness with any combination of implantation and post-implantation annealing. This is undoubtedly not because implantation has no effect on hardness, but because the large loads used cause indentations that far exceed the ion ranges (Table 1).

The results of these experiments are summarized in Figs. 1 to 3. In general, implantation with  $\text{Al}^+$  ions was more effective than implantation with  $\text{B}^+$  ions in increasing  $K_c$  of the  $\text{Si}_3\text{N}_4$ , though the increase in  $K_c$  exceeded 15 % in only two cases ( $\text{Al}^+$ -as-implanted to a dose of  $10^{16}$  and  $\text{Al}^+$  annealed at  $1100$  °C after implanting to  $2.5 \times 10^{16}$  ions/cm<sup>2</sup>). Co-implantation with  $\text{N}^+$  was done to higher total doses, and noticeably reduces the values of  $K_c$  in the as-implanted condition. However, annealing the  $\text{Al}^+$ -implanted  $\text{Si}_3\text{N}_4$  at  $1000$  °C increased  $K_c$  by about 18 % over that of unimplanted material, while the toughness of the  $\text{B}^+$ -implanted  $\text{Si}_3\text{N}_4$  increased by about the same amount on annealing at  $1100$  °C.

A second series of implantation experiments was performed on metallographically polished bars and disks of  $\text{Si}_3\text{N}_4$ . The disks were 3 mm in diameter and ranged in thickness from 250 to 500  $\mu\text{m}$ . The intent of these experiments was to perform controlled-flaw tests [6,7], which require indentation at specific loads prior to

testing, in preparation for testing in our miniaturized disk-bend testing apparatus [8]. The thinner disks were to be indented at lower loads, while the thicker ones were to be indented using larger loads (up to ~10 kg on our microhardness indentation machine). A summary of the irradiation conditions is presented in Table 2. Unfortunately, the grant period expired, the funds were exhausted, and it was not possible to complete the planned experiments on the mechanical behavior of the implanted disks.

#### References

1. B. R. Lawn, A. G. Evans and D. B. Marshall, *J. Amer. Ceram. Soc.* **63** (1980) 574.
2. D. K. Shetty, A. R. Rosenfield and W. H. Duckworth, *J. Amer. Ceram. Soc.* **68** (1985) C65.
3. R. F. Krause Jr., *J. Amer. Ceram. Soc.* **71** (1988) 338.
4. N. Ramachandran and D. K. Shetty, *J. Amer. Ceram. Soc.* **74** (1991) 2634.
5. R. F. Cook, C. J. Fairbanks, B. R. Lawn and Y.-W. Mai, *J. Mater. Res.* **2** (1987) 345.
6. J. Zhang and A. J. Ardell, *J. Amer. Ceram. Soc.* **76** (1993) 1340.
7. F. C. Chen, *J. Innov. Mater. Res.* **1** (1996) 47.
8. D. E. Meyers, F. C. Chen, J. Zhang and A. J. Ardell, *J. Test. Eval.* **21** (1993) 263.

Table 1. Ion implantation conditions for the initial experiments.

Ion Species	Ion Energy (keV)	Fluence (ions/cm <sup>2</sup> )	Range (nm)
Al	300	$10^{15}$	315
"	"	$10^{16}$	"
"	"	$2.5 \times 10^{16}$	"
Al	300	$2.5 \times 10^{16}$	315
+			
N	240	$2.5 \times 10^{16}$	"
B	300	$10^{15}$	540
"	"	$10^{16}$	"
B	200	$10^{16}$	385
+			
N	300	$10^{16}$	"

Table 2. Ion implantation conditions for the Si<sub>3</sub>N<sub>4</sub> disks and bars.

Specimen Type	Ion Species	Ion Energy (keV)	Fluence (ions/cm <sup>2</sup> )
3 × 5 mm bar and 32 disks	Al + N	Al: 300 N: 225	$2.5 \times 10^{16}$ each
3 × 5 mm bar and 32 disks	B + Al	B: 200 N: 300	$1.0 \times 10^{16}$ each
3 × 5 mm bar and 32 disks	Al	300	$2.5 \times 10^{16}$
16 disks	Al	300	$10^{16}$

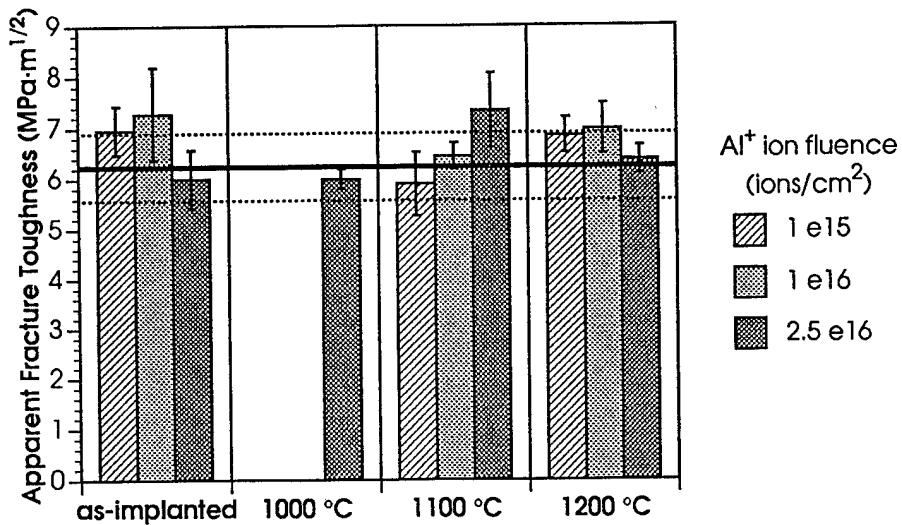


Figure 1. Apparent fracture toughness,  $K_c$ , of  $\text{Si}_3\text{N}_4$  after implantation of  $\text{Al}^+$  ions to the fluences indicated, and post-implantation annealing. The heavy horizontal line represents the average value of  $K_c$  of the as-received material, and the dashed lines the standard deviation. The  $\text{Si}_3\text{N}_4$  implanted with  $\text{Al}^+$  to the lower two doses was not annealed at 1000 °C.

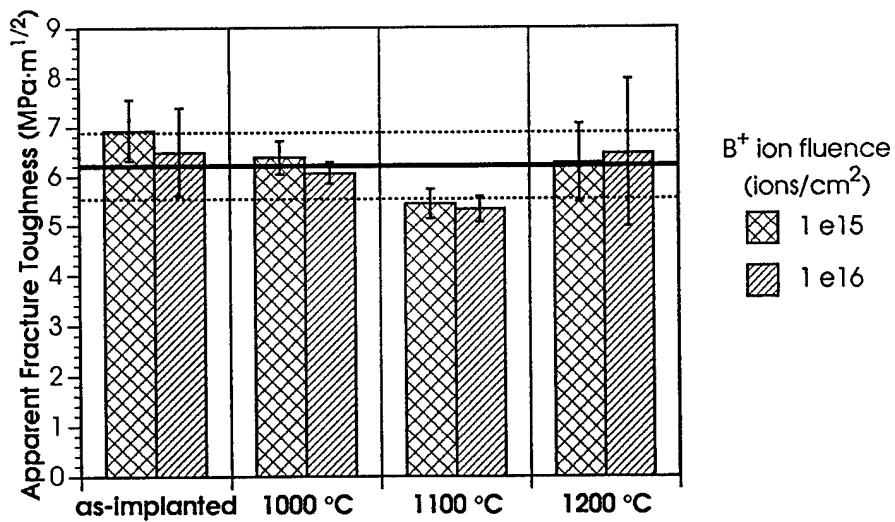


Figure 2. Apparent fracture toughness,  $K_c$ , of  $\text{Si}_3\text{N}_4$  after implantation of  $\text{B}^+$  ions to the fluences indicated, and post-implantation annealing.

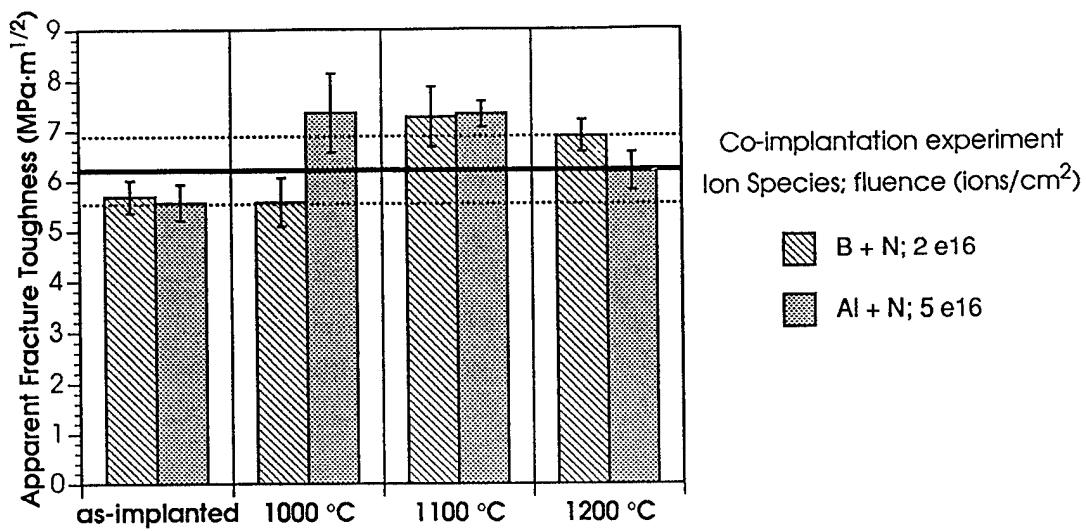


Figure 3. Apparent fracture toughness,  $K_c$ , of  $\text{Si}_3\text{N}_4$  after co-implantation of  $\text{Al}^+ + \text{N}^+$  and  $\text{B}^+ + \text{N}^+$  ions to the fluences indicated, and post-implantation annealing.